

75 cc Model

Surgin Arm Part Bearings, available

E 2127 350 x 500 BSA

$\frac{5}{8}$   $\frac{1}{10}$ ,  $1\frac{1}{4}$   $\frac{1}{10}$ ,  $2\frac{1}{4}$  length of outer sleeve.

$4\frac{11}{16}$  length of inner sleeve.

E 21210 650 BSA

$1\frac{3}{16}$   $\frac{1}{10}$ ,  $1\frac{1}{4}$   $\frac{1}{10}$ ,  $2\frac{1}{4}$  length of outer sleeve.

$4\frac{11}{16}$  length of inner sleeve.

Lengths can be modified.

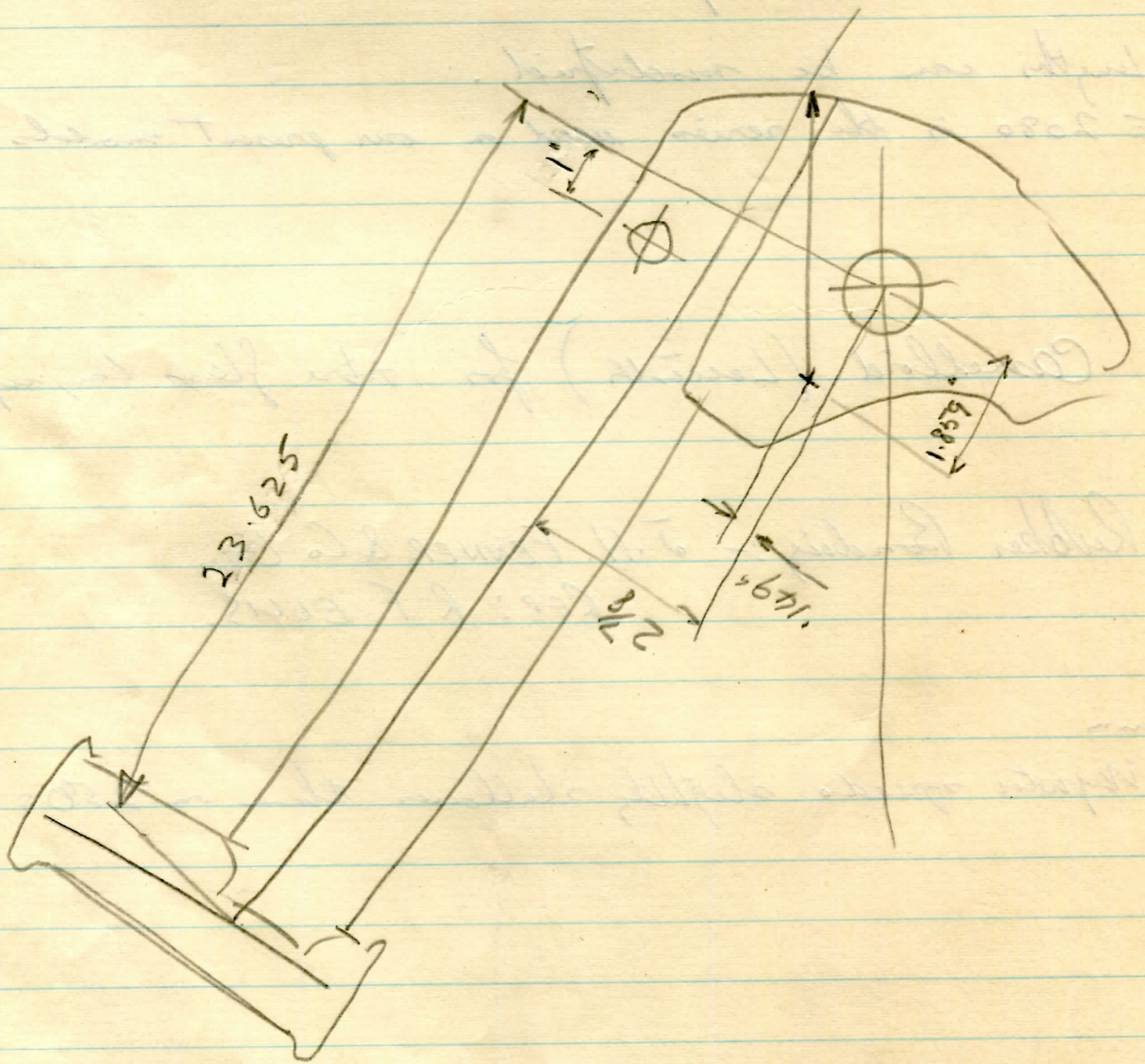
E 2080 in the series used on our present models

Carcelloid (Lecicor) for fibre glass lay up

Rubber Bonding: - J.H. FENNER & Co Ltd,  
Rep: R.F. ELLIS.

60 mm

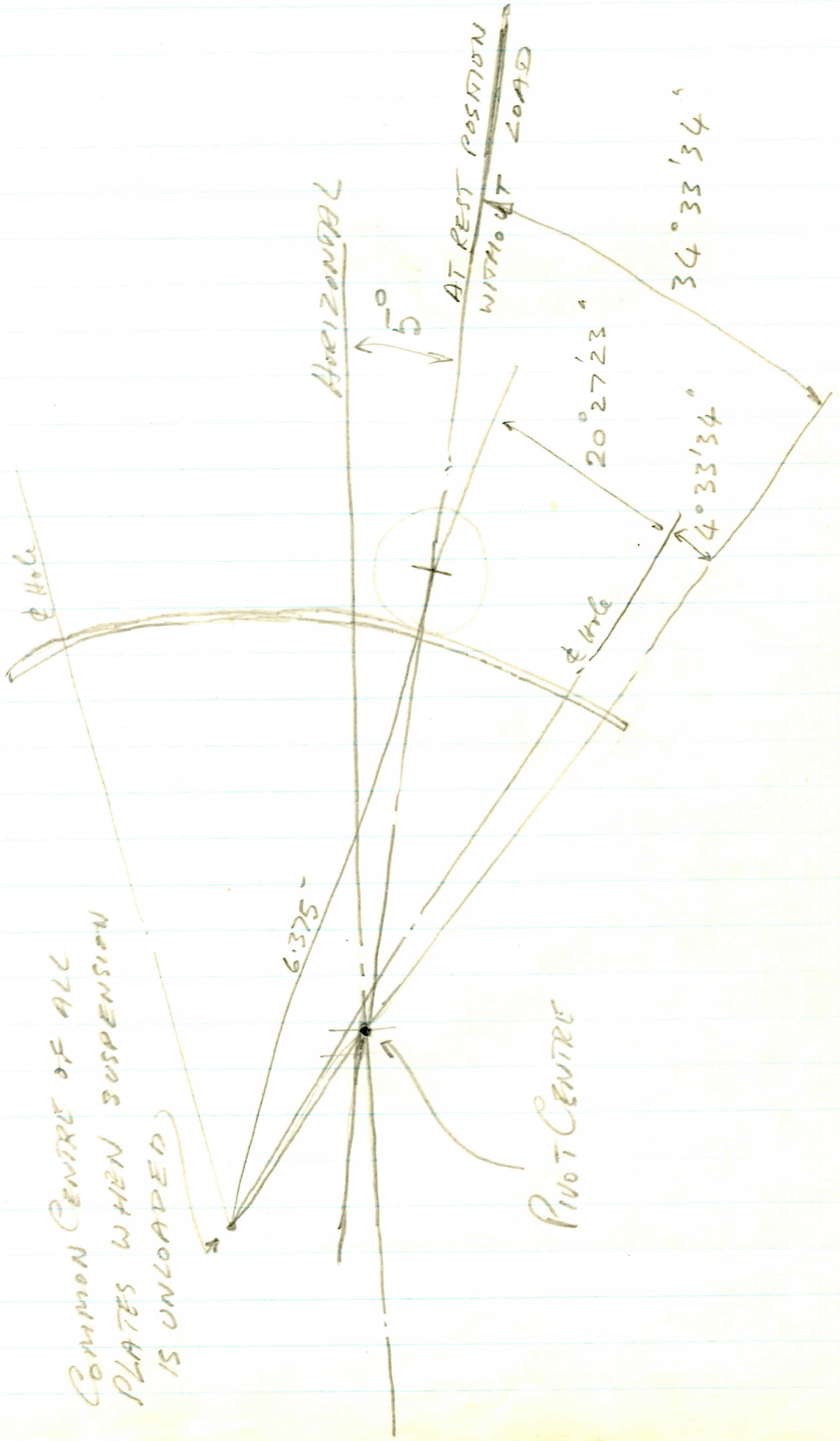
^ Maywater speeds slightly shallower than on 250s



FRAME

# RUBBER SUSPENSION UNIT

COMMON CENTRE OF ALL  
PLATES WHEN SUSPENSION  
IS UNLOADED



Prototype with 50cc engine

Rear chain line 2.056"

Rear Sprocket 30 teeth  
Width 176 / 168

°/Die ~~1230~~ 5.070"

Pitch Dia ~~4963~~ 4.783"

Ball Dia ~~1658~~ 4.478"  
~~1643~~ 4.468"

Rear Chain  $\frac{1}{2}$ " pitch x .305" dia roller. (Britax?)

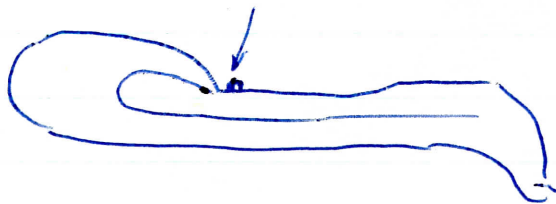
Sprocket patterned on Ensign W. 42794 but slightly thinner  
alters normal chainline of Ensign to the 2.056 (above)

Top Gear Ratio = ~~14.72~~ 14.72

Bottom " " = ~~26.38~~ 26.38

Fibreglass Body - Form rib to stop water

entering seat



6-8-63

Estimated Revs/mile of 17x2.50 Tyre = 919

Speedo drive is  $\frac{1}{2}$  speed of c'shaft sprocket.

With 38T Rear Sprocket, Speedo drive would do

$$\frac{38}{12} \times 919 \times \frac{1}{2} = \underline{1460} \text{ Revs/mile.}$$

(1490 if tyre gives 940 Revs/mile)

With 44T Rear Sprocket, Speedo drive would do

$$\frac{44}{12} \times 919 \times \frac{1}{2} = \underline{1690} \text{ Revs/mile}$$

(1725 if tyre gives 940 Revs/mile)

With speedo drive from Front Wheel 18:10 box would give 1658 Revs/mile on drive cable.

If Dunlop revs/mile are incorrect as Smiths have found to be the case on tests made on other sizes of ~~tyres~~ tyres then it is likely that 17x2.50 tyres might give 960 revs/mile and then 18:10 box would give 1692 Revs/mile on drive cable.

Red Fibre-Glass Body. - Inserts under seats were  $\frac{1}{8}$ " too far back, holes redrilled correctly.

### PRICES

TYRE, TUBE & RIM TAPE (complete)	250x17	37/6
	300x17	42/6
	2.25x17	39/8

Rim	WMI 17	8/2d each - <u>not plated</u>
	WMO 17	8/- " " " "

2-4-64 ~~M.P.I.~~ MOTORI-MORINI-FRANCO

80 cc 2-STROKE 4 SPEED ENGINE UNIT

45 mm BORE x 49 mm STROKE = 77.93 cc.

C.R. 8.5:1

5 BHP @ 6,800

Generator 28 W, 6 V.

Dell'orto UA 195 Carb.

Petrol Mixture 1:20

Sparking Plug CW 240 x 14 mm.

PRIMARY GEAR RATIO 1:3.1

<u>GEAR BOX RATIOS (INTERNAL)</u>	<u>ENGINE/FINAL DRIVE SPROCKET</u>
1ST :	1 : 3.3
2ND :	1 : 1.933
3RD :	1 : 1.529
TOP :	1 : 1.2

REAR CHAIN -  $\frac{1}{2}$ " PITCH x  $\frac{3}{16}$  WIDE x .305" dia roller.

FINAL DRIVE SPROCKET 14 T

REAR SPROCKET TO SUIT 19" x 2.75 REAR TYRE = 38

" " " 17" x 2.50 " " = 35

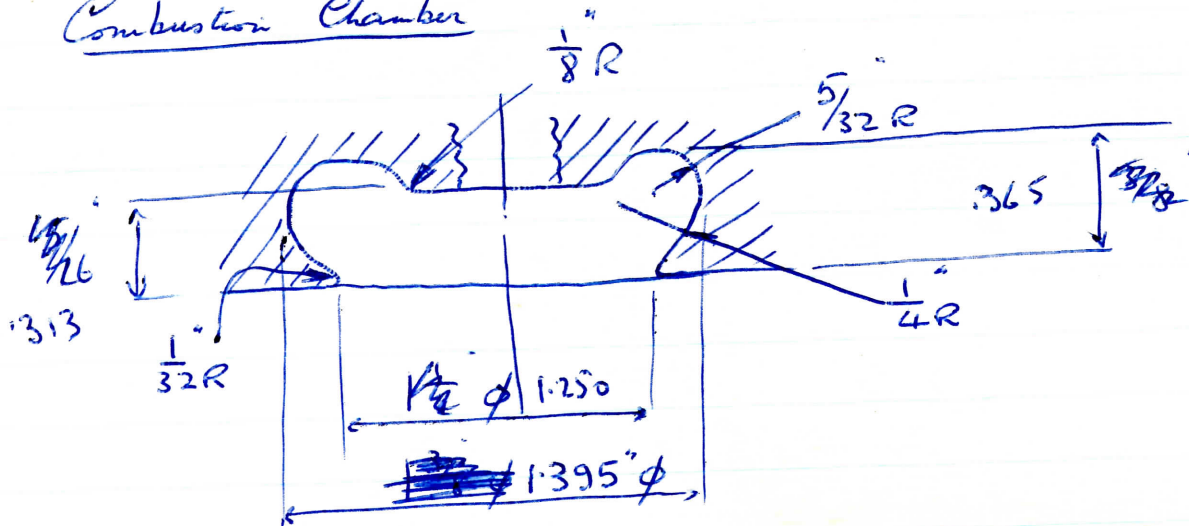
REAR CHAINLINE = 2.658 (ENGINE CENTRAL)

WEIGHT = 35.27 lbs

OIL CAPACITY = 1.43 p5.

# 75cc 2/STROKE ENGINE

## Combustion Chamber



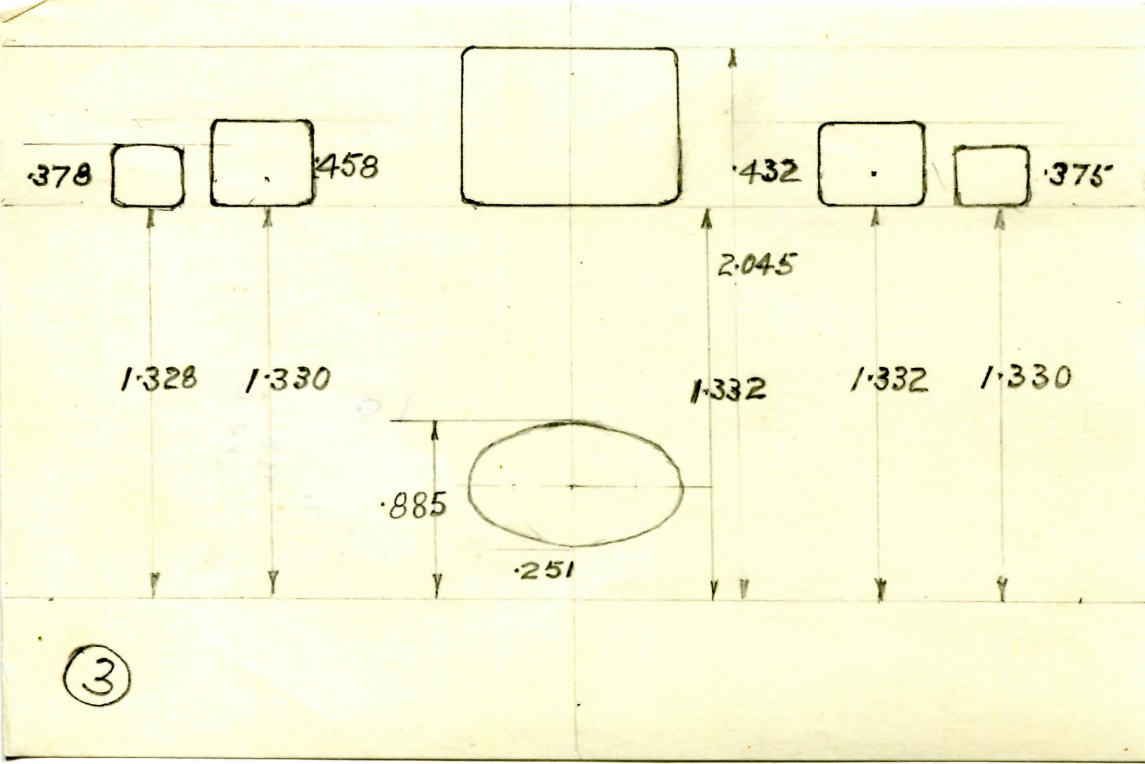
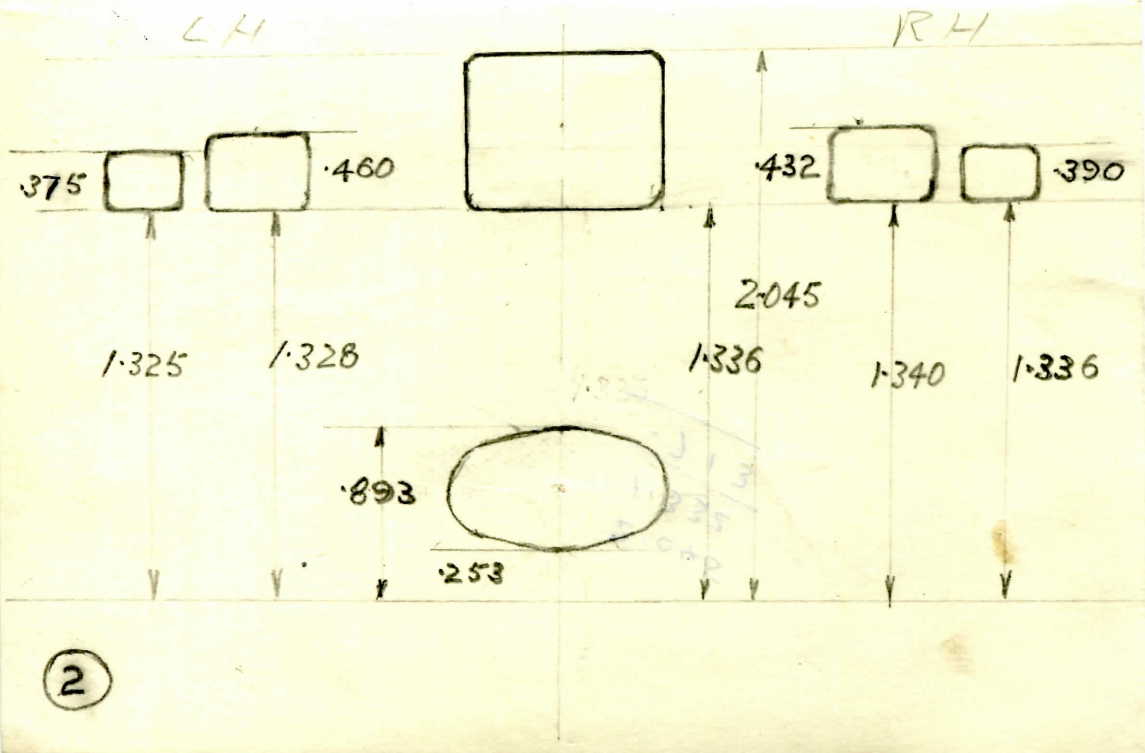
Sparky Plug. Lodge HH14

## Piston Dimensions

Top hand Die	= 1.917"
2nd " "	= 1.918"
Top of Skirt (Fore & aft)	= 1.924"
" " (across)	= 1.919"
Bot. " " (Fore & aft)	= 1.926"
" " (across)	= 1.921"
Height - overall	= 2.053"
Height to G/Pin	= .871"
Groove width	= .064"
" Bot. dia	= 1.715"
G/Pin Die	= .493"
" height	= 1.621"
" centre hole dia	= 1/4"
Ring width	= .063"
" section depth	= .070"

IGN TIMING 1/32" BEFORE T.D.C.

CYL. BASE GASKET .010" - .012" THICK



Iron Rod Total	3	12
Small End	1	10
Pin	5	3
Big End Leo Roller and Bracket Pin	2	2
" Complete	5	6

Weight of machine = 154 lbs + Rider (Hat = 156 lbs) ~~200 lbs~~ = 308 lbs

$$A = 40 \text{ lbs} / \text{Ton} \cdot \frac{40 \times 308}{2240} = \frac{12320}{2240} = 5 \frac{1}{2} \text{ lb}$$

$$R = 5.5 + .015 V^2$$

$$\text{B.H.P.} = \frac{1.47 V (5.5 + .015 V^2)}{550}$$

B.H.P.	$\frac{1.47 V}{550}$	V	V <sup>2</sup>	$.015 V^2$	R
1.525	.0802	30	900	13.5	19
2.2x3	.0935	35	1225	18.35	23.85
<b>3.45</b>	<b>.1070</b>	40	1600	24	29.5
4.311	.1202	45	2025	30.4	35.9
5.715	.1338	50	2500	37.5	43
<b>7.48</b>	<b>.1471</b>	55	3025	45.4	50.9
9.84	.1605	60	3600	54	59.5
11.95	.1738	65	4225	63.4	68.9
6.75	.1418	53	2809	42.14	47.64
7.1	.1442	54	2916	43.74	49.24

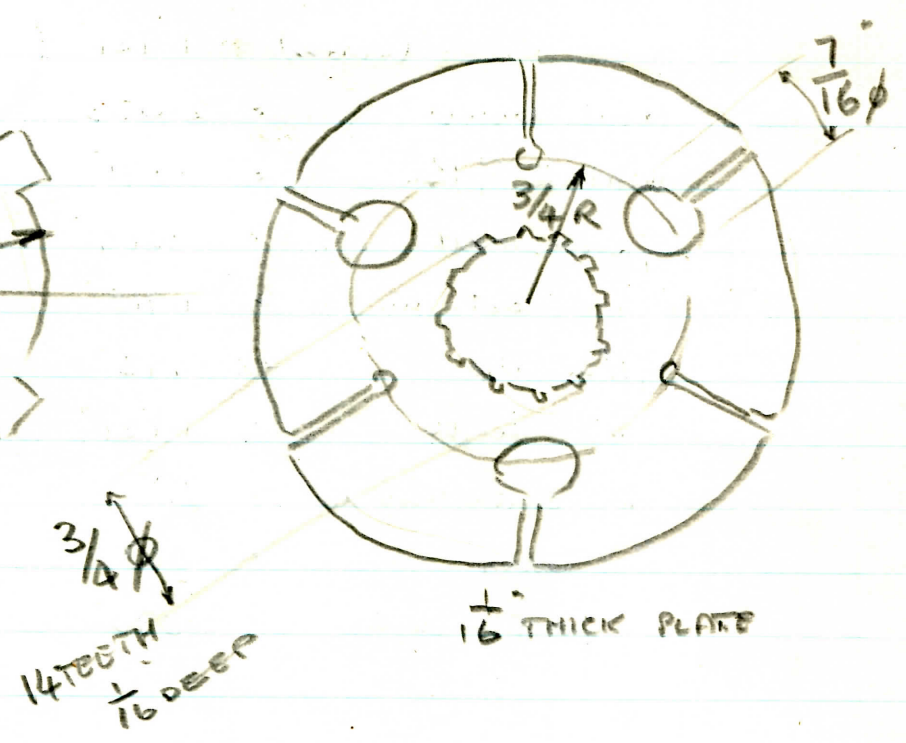
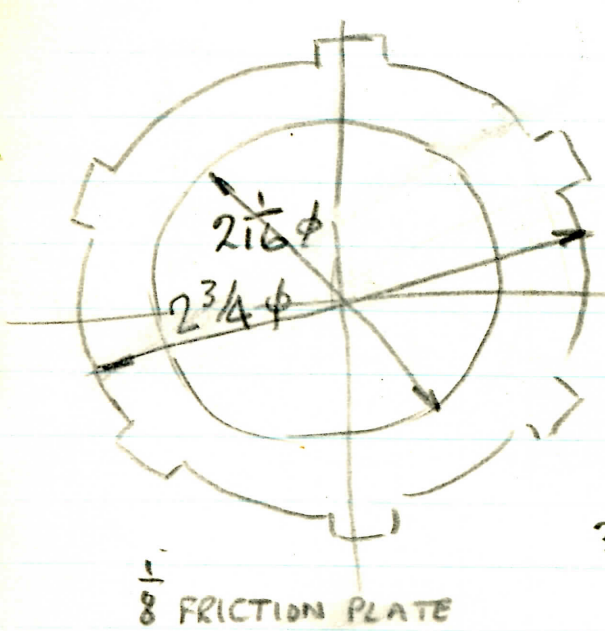
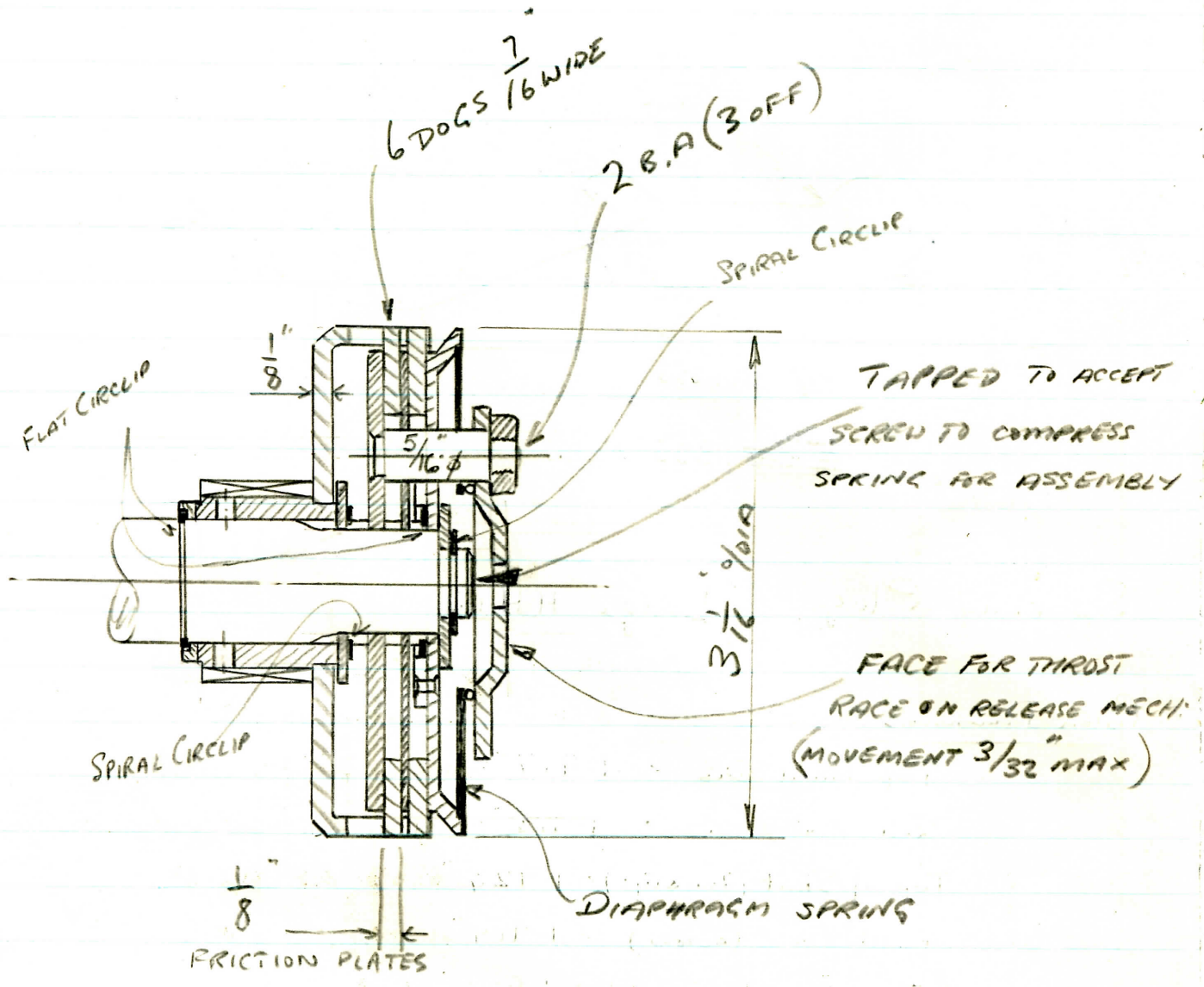
5 + 2x8 = 21

2.025	5.025	4.225
15	15	15
20250	30250	42250
10125	15125	21125
30375	45375	63375

502 14.7  
441  
55) 4.41 / .08

2.916
15
29160
14580
43740

2809
15
28090
14045
42135



ARMSTRONG SPRING BOXES

16-12-66

OTG/S-55018 - SERIAL NO C17 & C18

CHROME PLATED TOP COVERS.

With Cylinder Orifice hole .160" from top of cylinder  
and fitted with ATL/698 (75/110 lbs) Road Springs

12-2-65

Wiper Generator series 141 Output 21W or 24W

(MAX 28.8W)

(8W load & 200 test lamps should

be OK)

23-2-65

ARMSTRONG SPRING BOXES

RECEIVED 2 ROAD SPRINGS ATL/758 (60 lbs/in)

Sachs 97cc Engine / 4 speed unit

Crankshaft / Layshaft Ratio =  $14:34 = 2.43$

Layshaft / Mainshaft Ratios = .94 top

Overall Crankshaft / Final Drive Sprocket Ratios =

7.6; 4.11; 2.88; 2.3

Final Drive Sprocket 12T

Rear Chain  $\frac{1}{2}$ " x  $\frac{5}{16}$ " x .335" dia roller

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Rear Wheel Sprocket 36T = 6.89 top Ratio

= 53.75 mph @ 5,750 R.P.M.

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Weight 154 lbs + Rider.

956  
08

$$R = A + BV^2$$

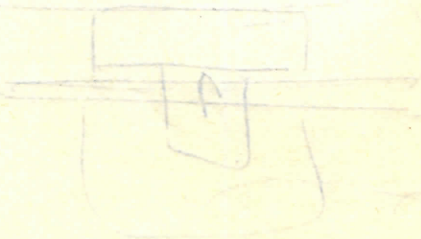
R = total resistance, lbs.

V = Speed, m.p.h.

A = a constant depending on laden weight and road conditions and type of tyre. (40 lbs per ton for pneumatics on concrete or tar-mac roads)

B = a constant depending on frontal area and degree of streamlining. (.014-.016 for motorcycles, rider prone no fairing.)

$$B.H.P. = \frac{1.47 V R}{550}$$



PRIMARY CHAIN 14T - 35T (OR LARGER)  
3/8" PITCH x .25" DIA ROLLER x .225" WIDE

FINAL SPROCKET 14T, .500" PITCH x .335" DIA ROLLER x .205" WIDE

REAR CHAINLINE 2 1/16"

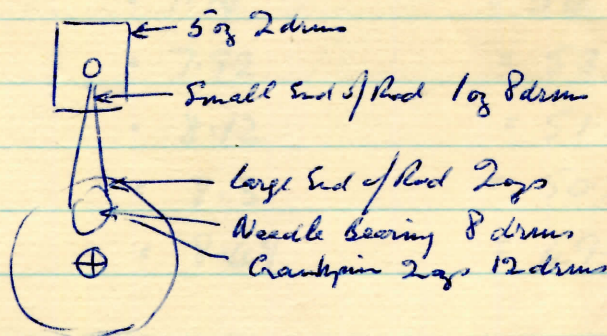
GEARBOX RATIOS 1, 1.25, 1.75, 3

100cc 50 in/l x 50 in/l = 98 1/4 cc 10-3-65

110 Piston Ref. 15347 { Compression Height 40.25 - /-  
to top of dome } Overall - 61.25 - /-  
9/Pi 12 - - φ

Estimated cost 15/-?

Balance (Estimated)



Piston etc, & Small end of rod = 6ozs 10drms.

50% balance = 3ozs 5drms.

3ozs 5drms + 2ozs + 8drms + 2ozs 12drms = 8ozs 9drms

= 4ozs 4 1/2 drms per wheel.

Crankpin hole saves 1oz 8drms leaving 2ozs 12 1/2 drms to balance in each wheel

2ozs 12 1/2 drms at .986" throw = 2.706 in/ozs. per wheel

100 cc

Primary Chain 14T-37T

$\frac{3}{8}$  pitch x 25 dia Roller x 225 wide x 50 pitches  
Centre Distance = 4.3747"

Rear Chain 14T-40T

$\frac{1}{2}$ " pitch x 335 dia Roller x 205 wide

Primary Chainline =  $3\frac{1}{16}$ "

Rear Chainline =  $2\frac{1}{16}$ "

Top Gear Ratio = 7.55 : 1

Rear Tyre = 17" x 2.50 = 932 Revs/mile.

= 55.5 mph at 6,500 & 59.7 mph at 7,000

37T Rear Sprocket	= 6.98	Top Gear	= 60 mph at 6,500
38T	= 7.17		= 58.5
39T	= 7.36		= 57
40T	= 7.55		= 55.5
41T	= 7.74		= 54
42T	= 7.92		= 53
43T	= 8.12		= 51.5
44T	= 8.3		= 50.5
45T	= 8.49		= 49.5

$$\left( \frac{\text{Engine speed in Revs/min}}{\text{Gear Ratio}} \times \frac{60}{\text{Revs/mile of Rear Wheel}} = \text{M.P.H.} \right)$$

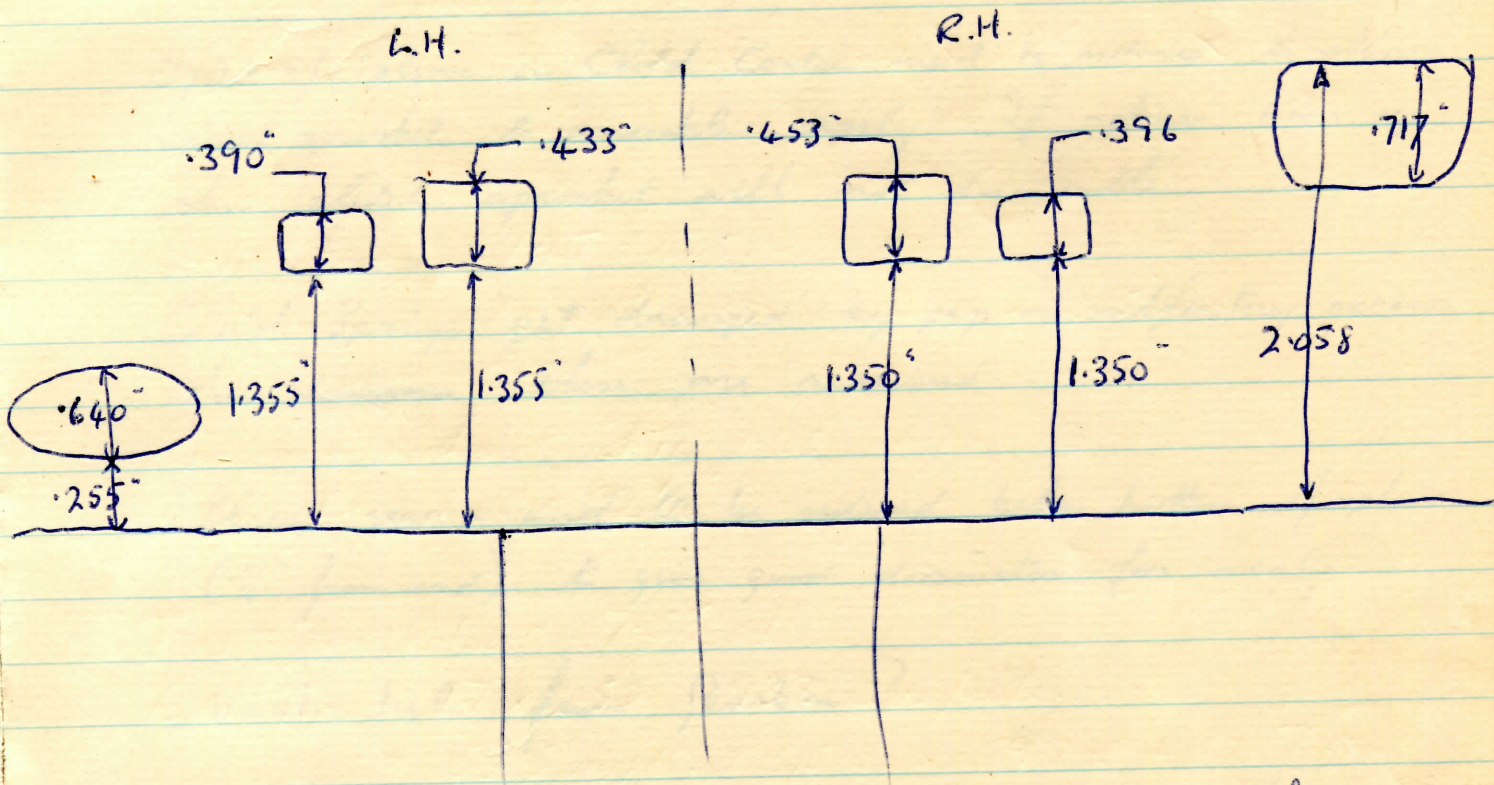
Gearbox Ratios = 1, 1.22, 1.475, 1.965, 2.92

Overall Ratios = 7.55, 9.21, 11.12, 14.83, 22.2

Volume of Crankcase (less Piston) up to Bottom of Ex Post = 215 cc  
 Volume of Piston Complete = 56 cc  
 Volume of Crankcase with Piston at Bottom of stroke = 159 cc

$$\text{Crankcase C.R.} = \frac{159 + 98}{159} = \frac{257}{159} = \underline{\underline{1.62}}$$

1st Prototype 98cc 2/stroke = 5 speed.



Port Dimensions as measured on 1st Barrel

Armstrong Reer Spring Boxes

23-9-65

OT6/S-55026

SERIAL NOS 65242/1 & 65242/2

Fitted with AT6/622 (60/120 lbs/in) Road Springs \*

ARM 5", STROKE 2"

Volume of Combustion Chamber = 12cc

$$C.R. = \frac{98 + 12}{12} = 9.17$$

Balance	Component	Weight	Count	Total
}	Corn Rod - Small End including Bush	1oz	10 drums	3oz 12 drums
	Big End - less Rollers & Crankpin	2oz	2 drums	
	Crankpin & Rollers	3oz	4 drums	5oz 6 drums
	Piston - with G/Pin & Circlips	5oz	3 drums	

11-10-65

Assembly of 1st Prototype 100cc Unit Construction 2/Stroke

O/Dia of Splines on Clutch Centre must be reduced to allow clutch sprocket to assemble easily. If splines burr up then clutch sprocket will not disassemble.

Clutch Springs get damaged by pip on adjusting screws when ~~down~~ these are removed.

Sleeve gear - end to be reduced below bottom of splines ( $\frac{1}{4}$ " from end) to give good diameter for seal.

Vent hole from Gearbox?

Pat alteration reqd. to prevent oil leaking from gearbox through Primary Chamber screw hole.

Shorter boss and stud for Gearbox Cover where foot-change lever spring fouls.

Final-drive Sprocket locking screws foul hex. of nut and recess in sprocket

Add 2 cable clips to engine for mag. wires.

Hole from grease nipple on Clutch lever-pivot to feed lower bearing in addition to top bearing.

Spring reqd. on Clutch lever pivot

Increase angle of piston ring gaps from  $30^\circ$  to  $35^\circ$  each side of  $\phi$

Oil flowing from clutch push rod hole in G/Box Cover.

11-11-65

Assembly of 1st Prototype 100cc Unit Construction 2/Stroke

Continued

Shorten Axial Induction Pipe by  $\frac{1}{4}$ "

Clutch Sprocket in too far, out of line with engine sprocket  
ø/DIA of Clutch centre ring (2.250") too large to fit  
2 $\frac{3}{16}$  dia recess in Clutch Back Plate

Centre distance between engine and gearbox mainshaft  
centres given as 4.376" by Messrs Reynolds Chassis

Alter position of Front Crankcase Dowel - Patts to be altered

Body prices

1 March 1966

3oz Body	2,000 off	5-19-4
	5,000	5-13-2
2oz Body	2,000	5-11-7
	5,000	5-5-11

Tool Charge £23 per 250 off

Nominal tool charge for developing ~~1~~ Tank bottom

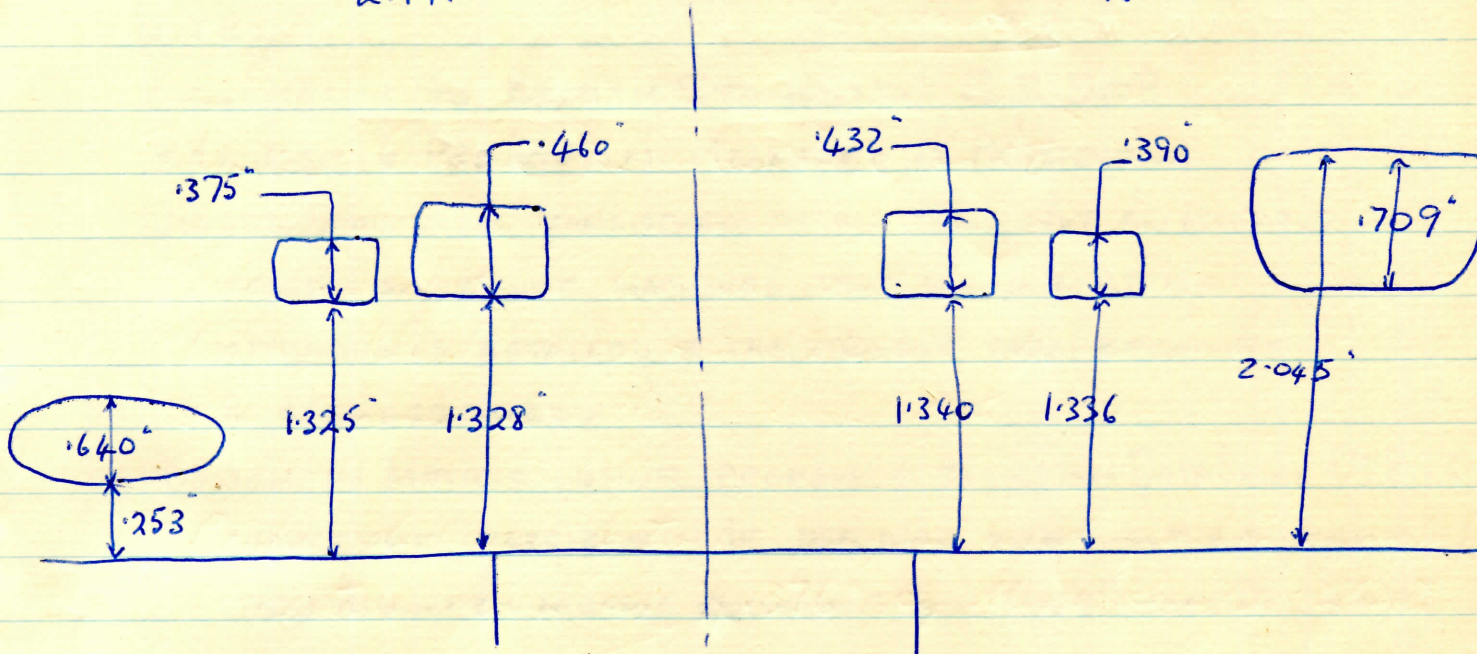
Enfield to supply 2 fixing pins & 2 Chrome  
Filter Cap.

N° 2 Barrel. 98 cc 2/Stroke - 5 speed

6/1/66

L.H.

R.H.



N° 3 Barrel 98 cc 2/Stroke - 5 speed

6/1/66

