

Dynamo Chain 48 Pitches 3.943" centre distance.

125 cc. Model RE-48.

30-12-47

The following prints given to Mr Pardoe for issue to George Neale or to Westwood :-

15 T. Mainshaft Pinion	34427 (7689m)	* Gear Change Adjusting Screw	34563 (7695m)
Mainshaft Spacing Collar.	34428	" " " " Banjo	34564 (RH) 34565 (LH)
* " Oil Retainer (Dr. Side)	34429	" " " Paul Carrier	34566 (7696m)
Gear Locating Plunger Body.	34430	" " " Paul	34567
* " " Plunger.	34431 (7690m)	* " " " Plunger	34568
* " " " Spring	34432	* " " " " Spring	34569
* 14 T. Final Drive Sprocket	34433	* " " Spindle Bush (T/Side)	34570 (7698m)
* 29 T Primary Driven "	34434	" " " Ratchet	34571
16 T Layshaft Pinion	34435 (7692m)	" " " Stop.	34572
21 T Mainshaft Sliding Pinion	34436	* " " Spindle Bush (D/Side)	34573
26 T " Pinion	34437	* " " Lever Return Spring	34574 (7699m)
Mainshaft	34438	* " " Return Lever	34575
Layshaft	34439 (7693m)	* " " Spindle	34576
27 T Layshaft Pinion	34440	* " " " (Complete)	34577
21 T " Sliding Pinion	34441	" " " Lever	34578 (7700m)
* Layshaft Bush (Short)	34442	" " " Arm	34579
Gear Change Ratchet Lever	34561 (7695m)	* " " Lever Stud	34580
* " " " " Nut	34562	* Mainshaft Thrust Washer	34583

Items marked * issued to George Neale. Items marked † on order. Rest to Westwood

125 cc Model RE. 49.

6-1-48

Print of Clutch Plate 34597 (7715m) given to Mr Pardoe to send to "Terodo" re. material.

125 cc Model RE-49.

Castings.

7-1-48

Clutch Worm Cover	34601 (7716m)	Pattern by Enfield.
Cylinder Head	34582 (7704m)	Dies by Lavender (No patterns)
Primary Chain Case	34581 (1406A)	Pattern by Dowler.
Crankcase (D/Side)	33663 (1404A)	" " "
" (T/Side)	33791 (1403A)	" " "

} Quotation Only.
Kickstarter Arr. not

125 cc Model RE-49.

16-1-48

Items marked * Issued to George Neale. Items marked ‡ on order.
Remainder issued to Westwood.

Crankshaft (Flywheel Side)	34584 (7705m)	Kickstarter Gear	34606 (7719m)
" (Driving Side)	34585 (")	" Spindle	34607 (")
Clutch Spring Plate	34589 (")	" Stop Plate	34608 (")
" Drum	34590 (")	‡ Clutch Spring	34617 (")
* " Thrust Member	34591 (7706m)	* Kickstarter Stop Plate Rivet	34609 (7720m)
* " " Assembly	34592 (")	* " Stop	34610 (")
* Driving Shaft Nut	34593 (")	" Pinion	34611 (")
* Engine Sprocket Roller	34594 (")	" Ratchet	34612 (")
* Clutch Worm	34599 (7716m)	* " Pinion Spindle	34613 (7721m)
" Operating lever	34600 (")	‡ " Bush	34614 (")
* Screwed Plug	34603 (7718m)	‡ " Ratchet Spring	34615 (")
* Bearing Spacer	34604 (")	‡ " Return	34616 (")
* Crankcase Seal Collar	34605 (")	* Clutch Thrust Member Disc	34602 (7723m)
* Spring Cap.	34618 (")	* " Plate Rivet	34619 (")
		* Engine Gear Unit Att. Nut (Front)	34620 (")
* Flywheel Hub (Miller Mag)	34701 (7734m)	Kickstarter Cover Backplate	34695 (7729m)
* Cam (")	34702 (")		

125 cc Model RE-49.

23-1-48.

GEAR CHANGE PEDAL 34766 (7723m) Issued to Westwood

125 cc Model RE-49

26-1-48

GEAR CHANGE TRUNNION 34772 (7734m) Issued to George Neale.

19-3-48

"J-47" 500cc. Single

Feed Pump. $\frac{1}{4}$ " dia plunger. $\frac{3}{8}$ " Stroke

= 1 pint per 22,596 revs. of Engine. (one side of pump only)

= 5.31 pints/hour at 2,000 revs/min. (" " " ")

496 cc. O.H.V. Vertical Twin.

Feed Pump. $\frac{1}{4}$ " dia. plunger. $\frac{1}{2}$ " Stroke.

12:1 reduction = 1 pint per 16,944 revs. of Engine (one side of pump only)

= 7.08 pints/hour at 2,000 revs/min. (" " " ")

9:1 reduction = 1 pint per 12,708 revs of Engine (one side of pump only)

= 9.44 pints/hour at 2,000 revs/min. (" " " ")

19-3-48

Oil Pump Worm Gearing.

Dr. No 3356 m. Single Start Worm & 18T Spindle

Centre distance = .6138" Ratio = 9:1 Helix Angle = $4^{\circ}56'38''$

2 start worm. Lead = $\frac{3}{16}$ " Worm wheel = 18T.

Existing Helix angle for single start = $2^{\circ}28'36''$

Centre distance = .6138" Ratio = 9:1

Worm 34995 (7701m)

2 Start Worm. Worm wheel = 18T - 34 DP.

Spindle 34996 (7701m)

Circular Pitch = .0924"

Pitch dia of worm wheel = .5294"

" " " Worm = .6982" % of Worm = .756

Helix angle of Worm = $4^{\circ}-49'$

Worm Plug 34997 (6728m)

23-3-48 Oil Pump Worm Gearing.

Centre distance = .614" Ratio = 6:1

Worm 35002 (6728m)

Worm: Double Threaded. 20° Pressure Angle Helix Angle = $6^{\circ}32'$

Pitch = .1309" Lead = .2618.

Top die = .8114"

Corrected Top die = .7865"

Pitch dia = .728"

Root dia = .6316"

" Root die = .6067"

Spindle 35003

Worm Wheel
Top die = 5834"

Corrected Top die = .6083"

(6728m)

496cc OHV. Vertical Twin.

6 April 48

Oil Release Valve (Crankshaft)

60 lbs \square " = 1.945 lbs on $\frac{13}{64}$ " dia.

$$F = \frac{8 P N D^3}{G d^4} = \frac{8 \times 1.945 \times 4 \times .222^3}{11,500,000 \times .028^4}$$

$$= \frac{.6722}{7.0679} = .095" \text{ deflection using spring } 26704 (5996 \text{ m})$$

11th May 1948

"G-2" Clearance between Driving Shaft Nut & Chaincase (Front half)
= .252"
.148"

Nut turned back $\frac{1}{16}$ " and 16 swg (.064") washer used giving $\frac{.253}{.145}$ " clearance for cork washer.

Use $\frac{1}{4}$ " thick cork washer. $\frac{15}{16}$ " bore. $\frac{13}{16}$ " o.d.

"TWIN" Clearance between crankshaft & chaincase (front half) = $\frac{.099}{.025}$ "

Recess crankshaft $1\frac{7}{32}$ " dia x $\frac{9}{64}$ " deep giving

.245" clearance for cork washer.

.161"

Use same washer as for "G-2"

31-5-48

125 cc. Stationary Engine (Base Fixing)

Attachment of Fan Cowling. 34460 (7703m)

2 Bosses at bottom $3\frac{5}{16}$ " down from \perp and 3" apart - $\frac{1}{2}$ " each side of \perp .
1 boss on vertical \perp $5\frac{1}{2}$ " up from main centre. Boss stands $\frac{3}{8}$ " back from outside face.

4 June 48. 98cc-14in Mower. (Old Type) (Sanction 824 m)

The following measurements taken from actual machines:-

$1\frac{11}{32}$ " from inside of R.H. Side plate to extreme end of ratchet pinion.

$1\frac{7}{32}$ " overall length of ratchet coupling.

$3\frac{31}{32}$ " from Engine to outside face of flywheel.

$7\frac{7}{8}$ " overall width of Engine.

$2\frac{3}{4}$ " from inside of R.H. Side plate to outside face of flywheel.

8 June 48 496 cc. OHV. TWIN.

Volume of Combustion chamber with flat topped piston = 46.8 cc.cms.

Compression Ratio with copper/ asbestos gasket & flat topped piston
= 6.3

With Standard 250 Bullet Piston 24216 (5395 m) = 7.1 Ratio

With Piston as 25057 (7697 m) but with $\frac{5}{32}$ " dome = 7.07 Ratio

" " " " " " $\frac{1}{8}$ " dome = 6.9 Ratio

" " " " " " .14" dome = 6.97 Ratio

" " " " " " .145" " = 7 Ratio

W.25064 in stock

Volume of Combustion chamber with .145" dome (7:1 Ratio) = 41.3 cc.cms.

25 June 48 496 cc. OHV. TWIN.

Volume of Combustion Chambers as measured by Mr Neale =

46.5 cc (6.3 Ratio) & 47.5 cc (6.2 Ratio)

One piston was .015" small on height of crown

∴ correct figure = 46.5 cc with .145" dome.

Volume of .145" dome = 5.5 cc.

" " $\frac{9}{32}$ " dome = 10.83 cc.

" " cut-aways to miss valves = .4 cc

∴ Volume of Combustion Chamber with $\frac{9}{32}$ " domed piston and copper/ asbestos gasket = $46.5 + 5.5 - 10.83 + .4 = 41.57$ cc

C.R. = $248 + 41.6 = 41.6 = \underline{\underline{6.96:1}}$

496 cc OHV. TWIN.

12/7/48

Volume of Combustion Chamber with flat top piston = 52 ccs.

Volume of $\frac{3}{16}$ " dome = 7.16 ccs.

Volume of cut-aways to miss valves = -16 ccs.

Volume of Combustion Chamber with $\frac{3}{16}$ " domed piston = 45 ccs.

Compression Ratio = 6.51:1

Volume of $\frac{3}{8}$ " dome = 14.65 ccs.

Volume of cut-aways to miss valves = -5 ccs.

Volume of Combustion Chamber with $\frac{3}{8}$ " domed piston = 37.85 ccs.

Compression Ratio = 7.55:1

$\frac{7}{16}$ dome gives 8:1

496 cc OHV TWIN.

31-8-48

Dynamo Sprocket 15T. W. 34420.

Overall length was .925" and length of bore was .826"

As fitted to prototypes. Dynamo was not to drawing.

Shaft of Dynamo $\frac{1}{8}$ " longer than drawing.

346 cc OHV. G-2"

4-10-48

Oil Pressure Valve Spring for Tappets.

Springs fitted to prototypes were made from carburettor springs.

Free length $1\frac{1}{4}$ " No. of active coils 12

Outside dia .193" Wire gauge = .022" (24 s w g)

Deflection should be .54" giving load on spring of 3.03 lbs
= pressure of 246 lbs/ \square "

For pressure of 50 lbs/ \square " spring load should be .615 lbs
= deflection of .109"

Volume of Combustion Chamber with flat top piston = 52 ccs.

Volume of $\frac{3}{16}$ " dome = 7.16 ccs.

Volume of cut-aways to miss valves = -16 ccs.

Volume of Combustion Chamber with $\frac{3}{16}$ " domed piston = 45 ccs.

Compression Ratio = 6.51:1

Volume of $\frac{3}{8}$ " dome = 14.65 ccs.

Volume of cut-aways to miss valves = -5 ccs.

Volume of Combustion Chamber with $\frac{3}{8}$ " domed piston = 37.85 ccs.

Compression Ratio = 7.55:1

$\frac{7}{16}$ dome gives 8:1

496 cc OHV TWIN.

31-8-48

Dynamo Sprocket 15T. W. 34420.

Overall length was .925" and length of bore was .826"

As fitted to prototypes. Dynamo was not to drawing.

Shaft of Dynamo $\frac{1}{8}$ " longer than drawing.

346 cc OHV "G-2"

4-10-48

Oil Pressure Valve Spring for Tappets.

Springs fitted to prototypes were made from cigarette springs.

Free length $1\frac{1}{4}$ " No of active coils 12

Outside dia .193" Wire gauge = .022" (24 swg)

Deflection should be .54" giving load on spring of 3.03 lbs

= pressure of 246 lbs/ \square "

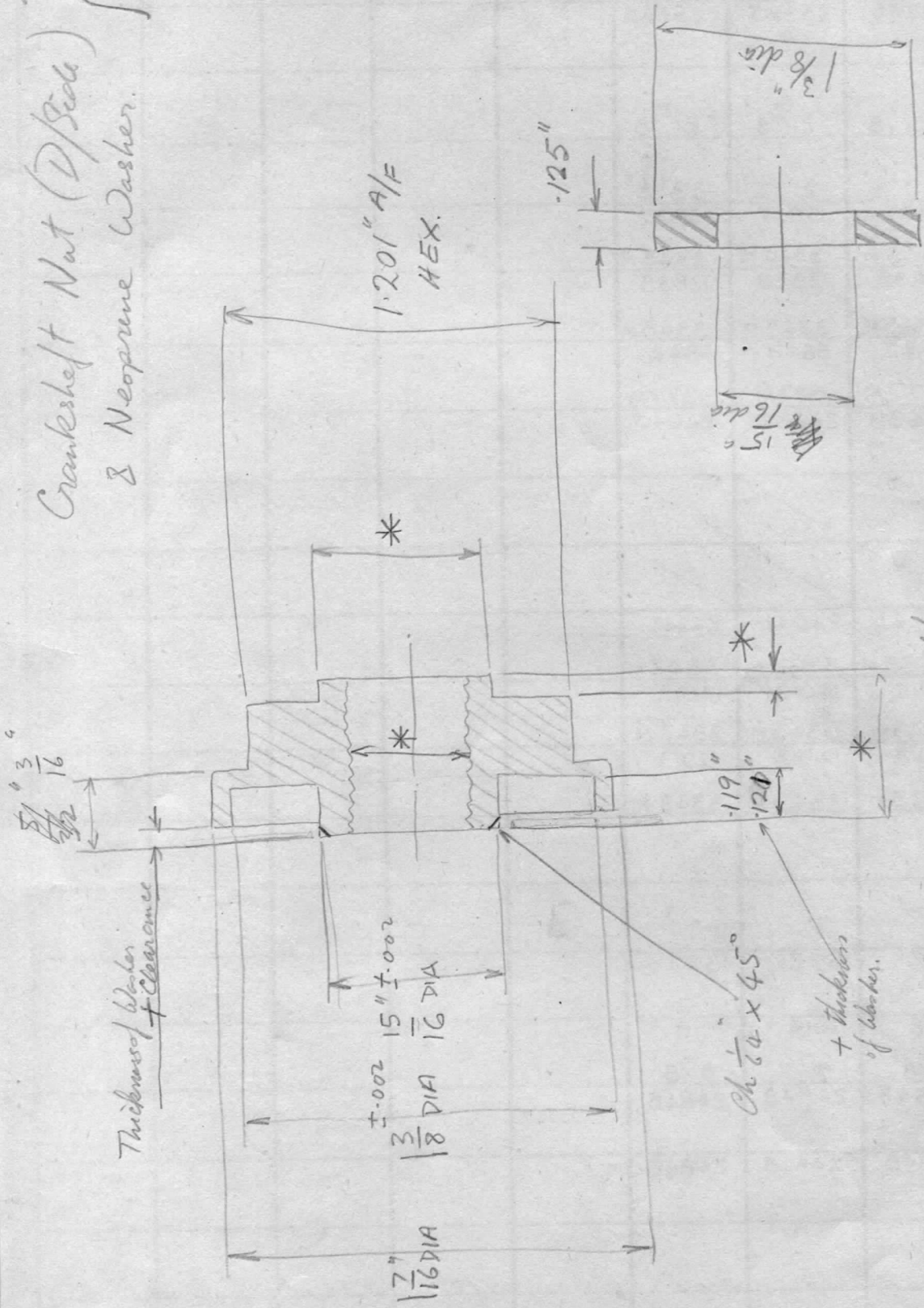
For pressure of 50 lbs/ \square " spring load should be .615 lbs

= deflection of .109"

With spring deflected .54" equal to load of 3.03 lbs, dia of hole to give 50 lbs/ \square " = $\frac{1}{4}$ " dia

Therefore Valve Seat must be sliding and spring has to support pressure on end of seat which is $\frac{1}{4}$ " dia. This accounts for stronger spring being necessary.

Crankshaft Nut (D/Slide) } RE-2
 & Neoprene Washer.



Neoprene. 10ff.

M.S. 10ff

Change
 in slot
 screw
 size
 its frame

as follows:-

Outside dia $3/16"$ Wire size $.018"$ (26 s.w.g.)

Free length = $.95"$ - 12 complete coils.

Ratio $C = 9.44$ $K = 1.15$ $S = 52,490$ $f = .020"$

125cc. MODEL R.E-2" 10-11-48

Drawings altered.

34593 (7706m)	34695 (7729m)	34574 (7699m)
34575 (7699m)	34576 (7699m)	34577 (7699m)
34578 (New Dwg N° 6859m)	34579 (New Dwg N° 6859m)	
34580 (7700m)	34403 (1405A)	34584 (7705m)
34701 (7734m)	34703 (7729m)	33791 (1403A)
34434 (7690m)	34438 (7692m)	34436 (7692m)
34610 (7720m)		

New Drawings.

35403 (6853m) Kickstarter Quadrant
35404 (lit 36D) Gear Change Spindle Washer.
35405 (6845m) Gear Change Centring Peg.
35411 (6859m) Gear Change Arm Spindle
35453 (6870m) Crankcase Sealing Bush (T/Side)

Schedule:- Add washer for Gear Change Spindle 35404

Add 1 off $1/4"$ shakerproof washer & 3 nuts 27622 (lit 1A) for Gear Change Arm & Lever.

Alterations Outstanding.

Crankcase (D/Side):- Move Gear box Filler hole towards centre. Use serrated screw with coin slot
Enlarge Carburettor hole to miss Screws. Plug for hole in line with Gear Change Arm Spindle needs "inking" into crankcase for ease of assembly of engine into frame

Primary Chaincase:- Thinner Walls, No. Drain Plug.

Use Crankshaft nut (D/Side) & Neoprene Washer etc. Lighten Clutch Op. Lever

First Clutch to be altered as prototype.

Gearbox Layshaft & Sliding Pinion to be altered.

Mainshaft & Sliding Pinion to be as previous to alteration.

Dwg of Flywheel Mag Hub & Crankshaft (T/Side) altered. If approved will affect design of new Lucas Flywheel mag

R-E Clutch 2 Feb 49

User Sprocket 35328

Insert Plate 35329

Distance on Clutch Driving Plate: $2\frac{9}{64}$ " from large end of taper to Clutch bearing face (as on 2nd Clutch)

Shorten thrust number 34591 by $\frac{1}{16}$ " and make allowance for thinner disc; thus dim $\frac{9}{16}$ " will be $\frac{5}{32}$ " and $\frac{7}{32}$ will be $\frac{1}{4}$ "

Disc 34602 will be $\frac{1}{32}$ " thick instead of $\frac{1}{16}$ "

No keyway in clutch Driving Plate

Shorter studs for extracting.

Particulars of keyway previously in Crankshaft (D/Side) 34585 (7705)

Keyway $\frac{1}{2}$ " dia x $.126$ " wide to suit Key W. 17504

$\frac{9}{32}$ " from large end of taper to $\&$ of keyway.

$\frac{5}{32}$ " from $\&$ Shaft to bottom of keyway.

G-2.

14-3-49

Distance between flywheel faces 2.632 "
 2.620 "

Distance from joint face to Gear Head (T/Side) 1.408 "
 1.404 "

" " " " Inner Bearing (D/Side) 1.447 "
 1.437 "

Distance between bearing faces (both cases) 2.855 "
 2.841 "

Thickness of T/Shaft Thrust Washer $.095$ "
 $.093$ "

" " D/Shaft " " $.112$ "
 $.110$ "

RE-2"

Gearbox

Tab Washer reqd. under Mainshaft Sprocket Nut.
Locked to Keyway in sprocket.

Sheep Proof Washer Used.



R.E-2"

18/3/49

Clutch. Driving Plate to be built up.

Spot Weld? ✓ Resistance Weld?

Serrate & rivet over similar to cycle crank and Sprocket?

Spot Weld

also spot weld boss and pressing for gearbox primary drive sprocket. X

Alteration to gearbox mainshaft or layshaft as on present R.E?

longer spring behind kickstarter ratchet ✓

Cancel old drawings X

3-5-49

Matl for Gear Change Arm 34579(6859m) EN34? ✓

R.E-2"

13/5/49

Crankshaft (Timing Side) to be redrawn or altered.

And to be shown on Arrangement. ✓

~~2nd gear position nearer to top?~~

~~This would mean allowing longer movement on bottom stop of Stop Plate and increasing the angle to first top tooth on ratchet.~~

Rectifier lighting Set RE-47

35964, 35961, 35962, 35963, 19068, 19069, 35965

35931, 35966, 26998, 27916, 24984, 35932, 27001, 27917

1 WIN

June 1st 1947

Width of Dynamo Chain $5/16 + 3/32$ movement. (Plates $3/32$ thick)

" " Camshaft Chain $15/32 + 1/16$ for spring links + $1/32$ movement.

$1/8$ " clearance between chains. $7/8$ " from face to outside dynamo chain.

$1 1/16$ " from face to inside cover.

Clearance between chains decreased to $1/16$ " to enable chain N° 110036 to be used. Length of chain reqd. = 38 pitches endless.

Centres = $100 \text{ mm} = 3.937" = 10 \frac{1}{2}$ pitches.

125 cc Stationary Engine with Mechanical Governor. 14-6-49

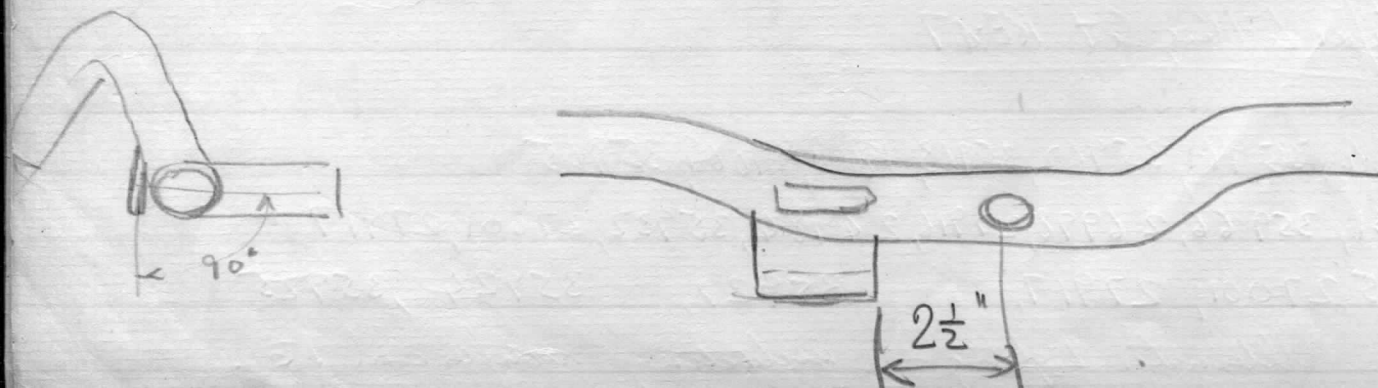
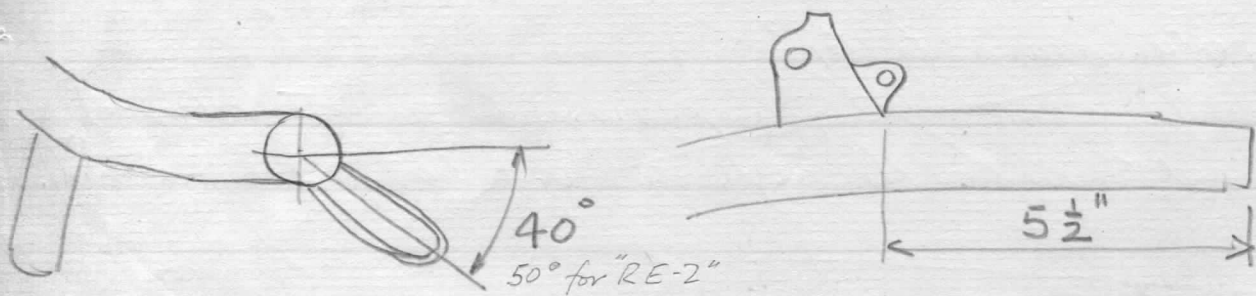
Gear Data - N° of Teeth = 14
 Normal D.P. = 24
 Angle of teeth = 45° L.H.
 O/D = .9084"
 Pitch Dia = .8250"
 Root Dia = .7286"

3-8-49

"G-2" Detachable Hub Details. 7515m, 7516m

RE Handlebars. Standard Bend.

9-8-49



25 ✓

D.O.

18.7.49

Model RE Handlebar
Sanction 889 m

Please note the following alterations
to schedule sheet 18 :-

1 off Clutch Cable Adjuster 35791 deleted
1 off " " " Locknut 7367 deleted
1 off " " Nipple (Clutch End) 35792 deleted
1 off " " Adjuster Screwed Bush 35761 deleted.

1 off Clutch Cable Nipple (Gearbox End) 3245 added.

These alterations are necessary
as these bars were originally
for the Model RE-2 but
are now for use on the
present Model RE.

Mr H. J. Gurse

Moment of Inertia of Bobweights on S-39 machine = 3.357 in/lbs.

(2 weights each 1.678 in/lbs)

Moment of Inertia of Bobweights on Cast Crankshaft = ~~3.97~~ 3.97 in/lbs
with bobweights each $1\frac{1}{32}$ " wide extending 180°

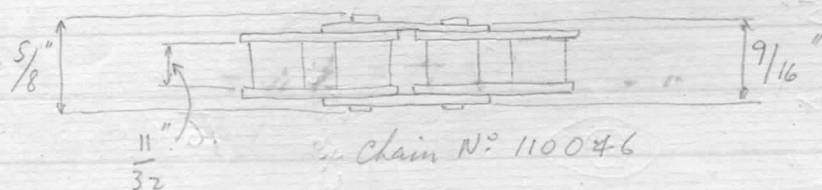
Sprocket Sizes Primary 17T — 36T

Final 17T — 50T Smaller for 24" wheel.

Length of Primary Chain = 50 pitches Chain N° 110046 .5" pitch

Primary Drive centres = 5.670" (52 pitches = 6.187" centres)

Distance of Primary Drive from ϕ of Engine = ~~3~~ $3\frac{5}{16}$ "



Timing Chain N° 114 500 8 mm Duplex.

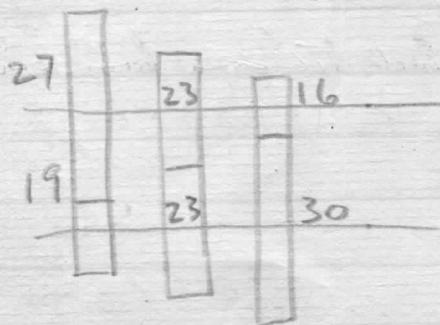
Engine Sprocket 14T. Camshaft Sprocket 28T.

Timing Drive Centres = 3.230" Length of Chain = 42 pitches

Distance from ϕ of Engine = ~~4~~ 4" (46 pitches = 3.875" centres)

Primary Drive - 54 pitches = 6.7016" centres

Gearbox



Bottom 16.5

2nd 8.81

Top 6.2

Gear Centres 1.918"
1.917"

12/14 Stub Teeth.

6.64
1.87

Gearbox with sleeve on layshaft.

Engine Speed 5000 - Gearbox mainshaft 2,361

Bottom Gear - layshaft & sleeve revolving together under load.

2nd Gear - layshaft speed 1,259 } difference in speeds 1,102
Sleeve speed 2,361 } (sleeve under load)

Top Gear - layshaft speed 1,259 } difference in speeds 2,096
Sleeve speed. 3,355 } (sleeve & shaft idling)

Jan 9th.

3.25-18 Tyre on WM2-18 Rim.

Sprocket size Primary 17T-36T
Final 17T-49T

Gear Ratios Bottom 16.25
2nd 8.67
Top 6-1

Jan 19th.

Chain N^o 110 036, 375" pitch x .25" Roller x .225"

Chain length 73 pitches

Engine Sprocket 23T Clutch Sprocket 50T

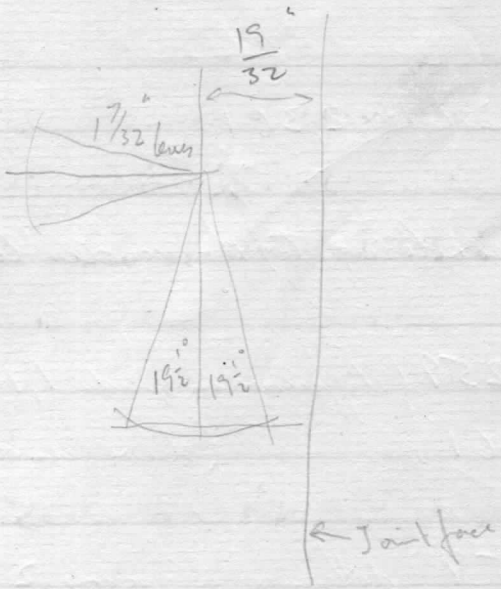
Centre Distance 6.645"

Engine sprocket 23T Clutch Sprocket 49T

Chain length 74 pitches Centre Distance 6.949"

23T: 50T 74 pitches C.D 6.838"

23T: 50T 74 pitches C.D 6.838"

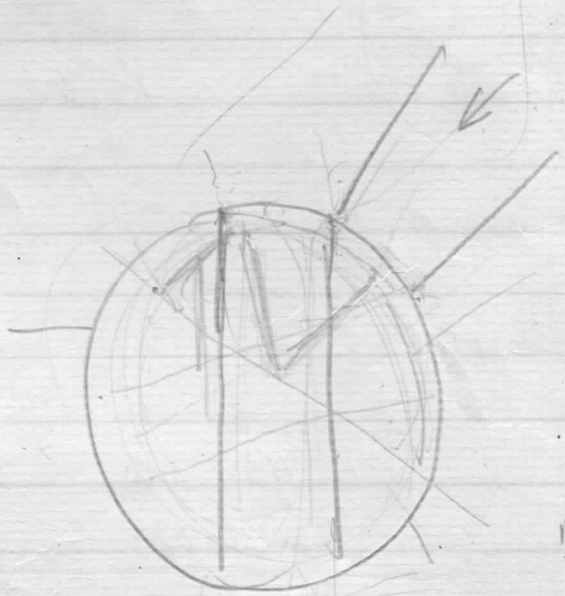


Gear locating Plunger Spring

78" Working length. 12 coils 199. (0.040")
 20" 1/0 Free length 1 1/8"
 Working load = 25 lbs.

178
 277
 564
 1880
 170
 170
 058656
 0276
 0862

1/16" + 1/16" 1/16"



4 36 257143
 29 128571
 302 385714
 100 192857
 200 140
 140 56
 56 28



135
 70
 1786
 062
 1927

1286
 2571
 2 3857
 192857

RE-2 Contact Breaker Cam.

0.010" Gap at Points = 43° Closed Period.

Jan 26th

Primary Chain. .375" pitch x .25" Roller x .225"
x 74 pitches (endless)
Engine Sprocket 23 T. } distance from $\frac{1}{2}$ Engine
Clutch " 49 T. } = 3 $\frac{7}{16}$ "

Rear chain
.500" pitch x .335" Roller x .305"

Gear Box Sprocket 17T
Rear Hub " 49T.

Gear Ratios with 3.25-18 Tyre on WM 2-18 Rim.
Bottom 16-33
2nd 8-72
Top 6-14

Gear Box. Mainshaft Gears 16T, 23T, 27T
Layshaft Gears 30T, 23T, 19T.

Gear Centres 1.918"
1.917" 12/14 Stub Teeth.

Timing Chain 8^m/in Duplex
Engine Sprocket 14T.
Camshaft " 28T.

length of Chain 46 pitches (endless)
Distance from $\frac{1}{2}$ Engine = 4 $\frac{7}{16}$ "

Kickstarter Gears:

18T & 36T 14 D.P. full depth.
= 1.9285" crs.

Breather Timing 80° after T.D.C. opens. 30 after T.D.C. open.

RE-2

7-3-50

Mr Hill of Albion Eng. Co. Ltd requested the following alterations -

W. 34568 } Silver Steel - Hardened & Tempered instead of

W. 34431 } M.S. C.H.

W. 35515 $\frac{3}{16} \times 32$ TPI instead of N° 3 BA.

W. 34433 " " " " " "

W. 36043 Small End of Taper opened out to $\frac{7}{16}$ " dia to enable them to use standard broach for keyway.

This shortens actual Taper to approx. $\frac{3}{8}$ " long.

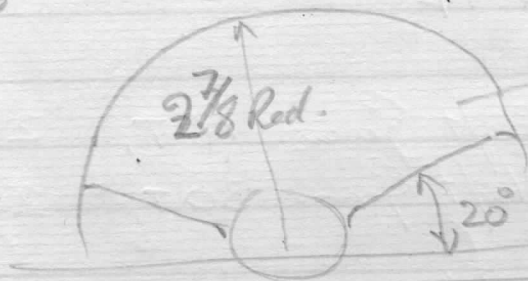
First few sets will be supplied with this modification.

22-3-50

Flywheel

$5\frac{3}{4}$ dia inside rim. Calculate Bobweights to 3.97 in/lbs

Bobweights



width .575" each flywheel

Kickstart Cover $\frac{1}{2}$ circle for Rubber Grommet

Hole for Rear Chain Guard Attachment.

1 Stud below Crankcase for attachment of Stand return Spring

Correct Breather Timing for longer Stroke.

Valves

Twin Springs etc.

Inlet as S.39

Check on length of Value Guides - Standards

Exhaust as Dia as Twin - length as S.39

Std Twin Piston.

Mar 31st

Pressure of oil at 6000 RPM required to overcome centrifugal force in feeding off-side main bearing
= $30 \frac{1}{2}$ lbs.

At 5000 RPM. = 21 lbs.

Pressure of oil required to continue feeding off-side main bearing after hole is filled with oil = 22 lbs at 6000 R.P.M.
& 15 lbs at 5,000 R.P.M.

May 12th

Top Dia of Kickstart Spline on Shaft = .729"

Valve Timings

E_2 opens. 60° before B.D.C.

- closes 22° after T.D.C.

K_1 opens. 22° before T.D.C.

- closes 60° after B.D.C.

Oil RELEASE VALVE (FROM CRANKSHAFT)

$60 \text{ lbs}/\square'' = 1.657 \text{ lbs on } \frac{3}{16}'' \text{ dia.}$

$$F = \frac{8 P N D^3}{G d^4} = \frac{8 \times 1.657 \times 4 \times .222^3}{11,500,000 \times .028^4} = \frac{.58014}{7.0685}$$

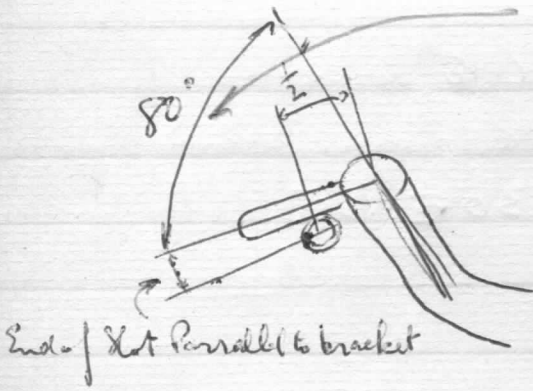
= .082" deflection using spring 26704 (5996m)

Note on Arrangement re. adjustment of Foot Change.

18-8-50

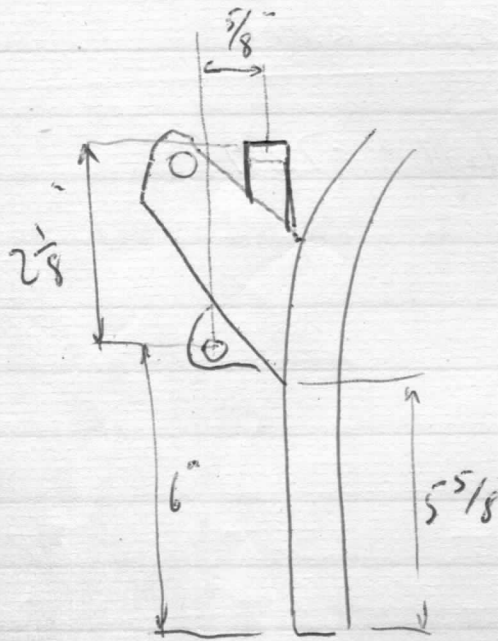
Positions of Brackets on Handlebars

This angle to be 70° - Mr Suisse.



End of Throttle Sleeve

End of Throttle Cable Stop = $3\frac{1}{2}$
 $3\frac{3}{8}$?



250 cc OHV. model

13-9-50

CLUTCH SPRINGS

12 H.P at 5,000 RPM = 2,347 RPM of CLUTCH

Allow 50% Safety factor = 18 HP AT 2,347

$$\frac{.32 \times 2\frac{3}{32} \times F \times 4 \times 2,347}{63,000} = 18$$

$$F = 186 \text{ lbs} = 62 \text{ lbs/spring (3 springs)}$$

13 swg (.092")

4 ^{effective} coils Free length = $1\frac{3}{16}$ " Inside dia = .51" dia

$$F = \frac{8PND^3}{6d^4} = \frac{8 \times 62 \times 4 \times .602^3}{11,500,000 \times .092^4} = .525" \text{ deflection}$$

Stress at Working length = 150,000

lbs/sq. in.